



# Bio-thermal convection caused by combined effects of swimming of oxytactic bacteria and inclined temperature gradient in a shallow fluid layer

Bio-thermal  
convection

157

Received 10 September 2008  
 Revised 1 December 2008  
 Accepted 15 December 2008

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## Abstract

**Purpose** – The aim of this paper is to investigate the onset of bio-thermal convection in a shallow fluid layer; the convection is thus driven by the combined effect of swimming of oxytactic microorganisms and inclined temperature gradient.

**Design/methodology/approach** – Linear stability analysis of the basic state is performed; the numerical problem is solved using the collocation method.

**Findings** – The most interesting outcome of this analysis is the correlation between three Rayleigh numbers, two traditional, “thermal” Rayleigh numbers, which are associated with the vertical and horizontal temperature gradients in the fluid layer, and the bioconvection Rayleigh number, which is associated with the density variation induced by the upswimming of microorganisms.

**Research limitations/implications** – Further research should address the application of weakly nonlinear analysis to this problem.

**Practical implications** – The increase of the horizontal thermal Rayleigh number stabilizes the basic flow. The effect of increasing the horizontal thermal Rayleigh number is to distort the basic temperature profile away from the linear one. The increase of the Schmidt number stabilizes the basic flow. The increase of the Prandtl number first causes the bioconvection Rayleigh number to decrease and then to increase.

**Originality/value** – To the best of the authors’ knowledge, this is the first research dealing with the effect of inclined temperature gradient on the stability of bioconvection.

**Keywords** Convection, Temperature distribution, Thermal stability, Fluids, Microbiology

**Paper type** Research paper

## Nomenclature

|               |  |                    |   |
|---------------|--|--------------------|---|
| $b$           | chemotaxis constant                                      | $\tilde{C}_{\min}$ | minimum dimensional oxygen concentration that microorganisms need in order to be active |
| $C$           | dimensionless oxygen concentration                       | $D_N$              | diffusivity of microorganisms   |
| $\tilde{C}$   | dimensional oxygen concentration defined in Equation (8) | $D_C$              | diffusivity of oxygen   |
| $\tilde{C}_0$ | free-surface dimensional oxygen concentration            | $g$                | gravity   |



|                    |   |   |   |
|--------------------|---|---|---|
| $G$                | rescaled dimensionless disturbance amplitude of oxygen concentration, $\Xi/\varsigma$   | $\tilde{T}_0$                           | ambient temperature   |
| $H$                | depth of the horizontal fluid layer   | $\tilde{u}, \tilde{v}, \tilde{w}$       | $\tilde{x}, \tilde{y}, \tilde{z}$ -velocity components, respectively  |
| $\hat{H}$          | heaviside step function   | $U_s, V_s, W_s$                         | $x, y, z$ -components of the dimensionless steady-state velocity, $\tilde{U}_s H \rho / \mu, \tilde{V}_s H \rho / \mu, \tilde{W}_s H \rho / \mu$ , respectively |
| $\tilde{j}$        | total flux of microorganisms due to macroscopic convection of the fluid, self-propelled swimming of microorganisms, and diffusion of microorganisms, $\tilde{n}\tilde{\mathbf{v}} + \tilde{n}\tilde{\mathbf{W}} - D_N \nabla \tilde{n}$ | $\tilde{U}_s, \tilde{V}_s, \tilde{W}_s$ | $\tilde{x}, \tilde{y}, \tilde{z}$ -components of the steady-state velocity, respectively  |
| $k, l$             | dimensionless wavenumbers in the $x$ - and $y$ -directions, respectively  | $\tilde{\mathbf{v}}$                    | fluid convection velocity vector ( $\tilde{u}, \tilde{v}, \tilde{w}$ )  |
| $\hat{\mathbf{k}}$ | vertically downward unit vector   | $W_c$                                   | parameter characterizing the maximum cell swimming speed  |
| $m$                | dimensionless wavenumber, $m^2 = k^2 + l^2$   | $\tilde{\mathbf{W}}$                    | average microorganisms' swimming velocity relative to the fluid, defined in Equation (7)  |
| $n$                | dimensionless number density of motile microorganisms, $\tilde{n}/n_0$  | $\tilde{x}, \tilde{y}, \tilde{z}$       | Cartesian coordinates ( $\tilde{z}$ is the downward vertical coordinate)  |
| $\tilde{n}$        | number density of motile microorganisms   | $x, y, z$                               | dimensionless Cartesian coordinates, $\tilde{x}/H, \tilde{y}/H$ , and $\tilde{z}/H$ , respectively  |
| $\tilde{n}_0$      | average number density of the microorganisms, defined in Equation (20)  | <i>Greek symbols</i>                    |   |
| $p$                | excess pressure (above hydrostatic)   | $\alpha$                                | thermal diffusivity of the suspension   |
| Pe                 | bioconvection Péclet number, $bW_c/D_N$   | $\beta$                                 | volumetric expansion coefficient of the fluid   |
| Pr                 | Prandtl number, $\mu/\alpha\rho_w$  | $\beta_H$                               | horizontal temperature gradient   |
| Ra <sub>B</sub>    | bioconvection Rayleigh number, $gH^3 \Delta\rho\theta\tilde{n}_0/\mu D_N$   | $\gamma$                                | rate of consumption of oxygen by the microorganisms   |
| Ra <sub>H</sub>    | horizontal thermal Rayleigh number, $g\beta H^4 \beta_H \rho_w / \mu \alpha$  | $\delta$                                | diffusion parameter, $D_C/D_N$  |
| Ra <sub>V</sub>    | vertical thermal Rayleigh number, $g\beta H^3 \Delta T \rho_w / \mu \alpha$   | $\Delta C$                              | difference between the free-surface and minimum oxygen concentrations, $\tilde{C}_0 - \tilde{C}_{\min}$   |
| Sc                 | Schmidt number, $\mu/D_N \rho_w$  | $\Delta T$                              | temperature difference between the lower and top surfaces measured at the same ( $\tilde{x}, \tilde{y}$ ) position  |
| $t$                | dimensionless time, $\tilde{t}\mu/\rho H^2$   |   |   |
| $\tilde{t}$        | time  |   |   |
| $T$                | dimensionless temperature, $(\tilde{T} - \tilde{T}_0)/\Delta T$   |   |   |
| $\tilde{T}$        | temperature   |   |   |

|               |   |             |  |
|---------------|---|-------------|--|
| $\Delta\rho$  | density difference, $\rho_{cell} - \rho_w$  | $\sigma$    | dimensionless disturbance frequency  |
| $\theta$      | average volume of a microorganism   | $\varsigma$ | dimensionless rate of consumption of oxygen by the microorganisms, $\gamma n_0 H^2 / D_C \Delta C$ |
| $\Theta$      | rescaled dimensionless disturbance amplitude of temperature, $\Omega(\alpha/D_N)$ | $\varpi$    | dimensionless parameter, $Pec$   |
| $\mu$         | dynamic viscosity   |             |  |
| $\rho_w$      | density of water  |             |  |
| $\rho_{cell}$ | density of cells  |             |  |

*Subscript*

s steady state

**1. Introduction**

Bioconvection is the spontaneous formation of macroscopic fluid patterns, such as falling plumes. It results from complex interaction of phenomena at different physical scales. The process is driven by the directional locomotion of self-propelled microorganisms that are denser than water; the swimming of each individual microorganism is a mesoscale physical phenomenon. The macroscopic density gradient caused by swimming of a large number of microorganisms (whose swimming velocity typically has an upward component) induces convection instability that results in the formation of a spatially periodic macroscopic fluid circulation.

The purpose of this paper is to investigate the interaction between bioconvection caused by motile oxytactic microorganisms, such as bacteria *Bacillus subtilis*, and natural convection caused by an inclined temperature gradient. The goal is to obtain a steady-state solution for a system subjected to an inclined temperature gradient and then investigate how the inclined temperature gradient affects the stability of this steady-state solution. The theory of oxytactic bioconvection was developed in Hillesdon *et al.* (1995), Hillesdon and Pedley (1996), and Metcalfe and Pedley (1998, 2001). Becker *et al.* (2004) extended this theory to oxytactic bioconvection in porous media and Avramenko and Kuznetsov (2005) investigated the onset of oxytactic bioconvection in superimposed fluid and porous layers. Kuznetsov (2005a, b) introduced the theory of bio-thermal convection caused by the combined effect of vertical temperature gradient and the upswimming of oxytactic microorganisms in clear fluids, Kuznetsov (2006a) extended this theory to bio-thermal convection in porous media, and Kuznetsov (2006b) investigated the effect of high-frequency vibration on the onset of oxytactic bioconvection.

The instability problem of natural convection in a fluid layer of finite depth induced by the inclined temperature gradient was first investigated by Weber (1973, 1978). Nield (2004) reformulated the linear stability analysis for the inclined temperature gradient problem to lift the restrictions on the range of the Prandtl number. Recent advances in convection problems associated with an inclined temperature gradient are documented in Kaloni and Lou (2002, 2005), who considered extensions of this problem to Oldroyd-B and viscoelastic fluids; and Shklyaev and Nepomnyashchy (2004), who studied the stability of thermocapillary flows generated by an inclined temperature gradient. Recently, Avramenko and Kuznetsov (2010) investigated a combined bioconvection and thermal instability problem in a horizontal layer of finite depth with a basic temperature gradient inclined to the vertical, so that the basic flow (driven by the horizontal component of temperature gradient) is a single cell – the Hadley circulation. In Avramenko and Kuznetsov (2010), the suspension consisting of gyrotactic motile microorganisms was considered. The purpose of this paper is to investigate the onset of

bio-thermal convection in a suspension of oxytactic microorganisms, such as bacteria *Bacillus subtilis*, in a fluid layer with an inclined temperature gradient.

It is assumed that the inclined temperature gradient is moderate, so that the temperature variation does not kill the microorganisms and does not affect their oxytactic behavior. The dependence of the solubility of oxygen in water on the temperature is neglected. Oxytactic bacteria require oxygen for their metabolism and swim up the oxygen gradients. They require a minimum oxygen concentration,  $\tilde{C}_{\min}$ , in order to be active. Since this paper deals with a shallow layer, it is assumed that even at the bottom of the layer the oxygen concentration is larger than the minimum concentration.

## 2. Governing equations

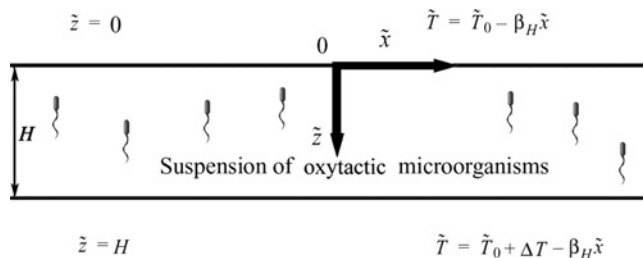
The model for bioconvection used in this study is based on that presented in Hillesdon *et al.* (1995), Hillesdon and Pedley (1996), and Metcalfe and Pedley (1998, 2001). This model is supplemented by an energy equation and a buoyancy term in the momentum equation that results from the inclined temperature gradient. The geometry of the problem is similar to that considered in Nield (2004) (see Figure 1). The suspension of oxytactic microorganisms is confined in a shallow horizontal box with small height-to-length and height-to-width aspect ratios. The two horizontal walls of the box are at a distance  $H$  apart. A Cartesian coordinate system  $(\tilde{x}, \tilde{y}, \tilde{z})$  (with the  $\tilde{z}$ -axis vertically downward) is chosen such that its origin is in the middle of the box. A linear horizontal temperature gradient is imposed in the  $\tilde{x}$ -direction, and a constant temperature difference is imposed between the two horizontal walls. The situation described above can be realized in a carefully planned lab experiment. The Boussinesq approximation is utilized. Under these assumptions, the governing equations are presented as:

$$\rho_w \left( \frac{\partial \tilde{\mathbf{v}}}{\partial \tilde{t}} + (\tilde{\mathbf{v}} \nabla) \tilde{\mathbf{v}} \right) = -\nabla p + \mu \nabla^2 \tilde{\mathbf{v}} + \hat{\mathbf{k}}(n\theta \Delta \rho g - \rho_w g \beta (\tilde{T} - \tilde{T}_0)) \quad (1)$$

$$\text{div}(\tilde{\mathbf{v}}) = 0 \quad (2)$$

$$\frac{\partial \tilde{n}}{\partial \tilde{t}} = -\text{div}(\tilde{\mathbf{j}}) \quad (3)$$

$$\frac{\partial \tilde{T}}{\partial \tilde{t}} + (\tilde{\mathbf{v}} \nabla) \tilde{T} = \alpha \nabla^2 \tilde{T} \quad (4)$$



**Figure 1.**  
Definition sketch

$$\frac{\partial C}{\partial \tilde{t}} + (\tilde{\mathbf{v}} \nabla) C = D_C \nabla^2 C - \frac{\gamma \tilde{\mathbf{n}}}{\Delta C} \quad (5)$$

where the total flux of microorganisms due to macroscopic convection of the fluid, self-propelled swimming of microorganisms, and diffusion of microorganisms is given by:

$$\tilde{\mathbf{j}} = \tilde{\mathbf{n}} \tilde{\mathbf{v}} + \tilde{\mathbf{n}} \tilde{\mathbf{W}} - D_N \nabla \tilde{\mathbf{n}} \quad (6)$$

where  $D_N$  is the diffusivity of microorganisms;  $g$  is the gravity;  $\tilde{\mathbf{n}}$  is the number density of motile microorganisms;  $\tilde{T}$  is the temperature;  $\tilde{T}_0$  is the ambient temperature;  $p$  is the excess pressure (above hydrostatic);  $\hat{\mathbf{k}}$  is the vertically downward unit vector;  $\tilde{t}$  is the time;  $\tilde{\mathbf{v}}$  is the fluid convection velocity vector with components  $\tilde{u}$ ,  $\tilde{v}$ ,  $\tilde{w}$ ;  $\theta$  is the average volume of a microorganism;  $\beta$  is the volumetric expansion coefficient of the fluid;  $\mu$  is the dynamic viscosity, assumed to be approximately the same as that of water;  $\Delta \rho = \rho_{cell} - \rho_w$  is the density difference;  $\rho_w$  is the density of water;  $\rho_{cell}$  is the density of cells;  $D_C$  is the diffusivity of oxygen; and  $-\gamma \tilde{\mathbf{n}} / \Delta C$  describes the consumption of oxygen by the microorganisms in the fluid.

The average directional swimming velocity of a microorganism is approximated as (Hillesdon and Pedley, 1996):

$$\tilde{\mathbf{W}} = b W_c \hat{\mathbf{H}}(C) \nabla C \quad (7)$$

where  $b$  is the chemotaxis constant (m) and  $W_c$  is a parameter characterizing the maximum cell swimming speed (m/s) (the product  $b W_c$  is assumed to be constant). The dimensionless oxygen concentration,  $C$ , in Equations (5) and (7) is defined as:

$$C = \frac{\tilde{C} - \tilde{C}_{\min}}{\tilde{C}_0 - \tilde{C}_{\min}} = \frac{\tilde{C} - \tilde{C}_{\min}}{\Delta C} \quad (8)$$

where  $\tilde{C}$  is the dimensional oxygen concentration,  $\tilde{C}_0$  is the free-surface dimensional oxygen concentration, and  $\tilde{C}_{\min}$  is the minimum dimensional oxygen concentration that microorganisms need in order to be active. Since for the shallow layer  $C > 0$  throughout the layer thickness, the Heaviside step function,  $\hat{\mathbf{H}}(C)$ , in Equation (7) is equal to unity.

### 3. Boundary conditions

As in Nield (2004), the ratio of the height to the length of the layer is assumed to be sufficiently small so that fluid motion in the horizontally central part of the box is not affected by lateral end effects.

If the top surface is rigid, the following conditions are satisfied there:

$$\tilde{\mathbf{v}} = 0, \quad \tilde{T} = \tilde{T}_0 - \beta_H \tilde{x}, \quad C = 1, \quad \tilde{\mathbf{j}} \cdot \hat{\mathbf{k}} = 0 \quad \text{at } \tilde{z} = 0 \quad (9)$$

where  $\beta_H$  is the constant horizontal temperature gradient.

If the top surface is stress-free, the first equation in (9) must be replaced with the following two equations:

$$\frac{\partial^2(\mathbf{v}\mathbf{k})}{\partial \tilde{z}^2} = 0, \quad \tilde{\mathbf{v}} \cdot \hat{\mathbf{k}} = 0 \quad (10)$$

The last equation in (9) ( $\tilde{\mathbf{j}} \cdot \hat{\mathbf{k}} = 0$ ) can be recast as:

$$\tilde{n}bW_c \frac{\partial C}{\partial \tilde{z}} - D_N \frac{\partial \tilde{n}}{\partial \tilde{z}} = 0 \quad (11)$$

At the bottom of the layer (assumed to be rigid) the following conditions are satisfied:

$$\tilde{\mathbf{v}} = 0, \quad \tilde{T} = \tilde{T}_0 + \Delta T - \beta_H \tilde{x}, \quad \frac{\partial C}{\partial \tilde{z}} = 0, \quad \tilde{\mathbf{j}} \cdot \hat{\mathbf{k}} = 0 \quad \text{at } \tilde{z} = 1 \quad (12)$$

The last equation in (12) ( $\tilde{\mathbf{j}} \cdot \hat{\mathbf{k}} = 0$ ), accounting for  $\partial C / \partial \tilde{z} = 0$ , can be recast as:

$$\frac{\partial \tilde{n}}{\partial \tilde{z}} = 0 \quad (13)$$

#### 4. Steady-state solution

From Equations (1)-(5) and the fact that the layer is infinite in the horizontal directions it follows that at steady state the number density of microorganisms,  $\tilde{n}_s$ , is a function of the vertical coordinate only; under this condition the steady-state solutions for the temperature and velocity components are, respectively (Nield, 2004):

$$T_s = z - \frac{1}{2} - \frac{\text{Ra}_H^2}{\text{Ra}_V} x - \frac{\text{Ra}_H^2}{5,760\text{Ra}_V} \left( 7 \left( z - \frac{1}{2} \right) - 40 \left( z - \frac{1}{2} \right)^3 + 48 \left( z - \frac{1}{2} \right)^5 \right), \quad (14)$$

$$U_s = -\frac{\text{Ra}_H}{24\text{Pr}} \left( \left( z - \frac{1}{2} \right) - 4 \left( z - \frac{1}{2} \right)^3 \right), \quad V_s = W_s = 0 \quad (15)$$

where the dimensionless  $\tilde{x}$  and  $\tilde{z}$  coordinates, steady-state temperature, and velocity components are defined by the following equations, respectively:

$$x = \tilde{x}/H, \quad z = \tilde{z}/H, \quad T_s = \frac{\tilde{T}_s - \tilde{T}_0}{\Delta T}, \quad U_s = \frac{\tilde{U}_s H \rho}{\mu}, \quad V_s = \frac{\tilde{V}_s H \rho}{\mu}, \quad W_s = \frac{\tilde{W}_s H \rho}{\mu} \quad (16)$$

and the vertical thermal Rayleigh number, horizontal thermal Rayleigh number, and Prandtl number are defined, respectively, as:

$$\text{Ra}_V = \frac{g\beta H^3 \Delta T \rho_w}{\mu \alpha}, \quad \text{Ra}_H = \frac{g\beta H^4 \beta_H \rho_w}{\mu \alpha}, \quad \text{Pr} = \frac{\mu}{\alpha \rho_w} \quad (17)$$

The steady-state solutions for  $C_s$  and  $\tilde{n}_s$  are found in Hillesdon *et al.* (1995) as follows:

$$C_s = 1 - \frac{2}{\text{Pe}} \ln \frac{\cos(A_1(1-z)/2)}{\cos(A_1/2)} \quad (18)$$

$$n_s = \frac{A_1}{2\text{Pe}\varsigma} \sec^2(A_1(1-z)/2) \quad (19)$$

where,

$$\text{Pe} = \frac{bW_c}{D_N}, \quad n_s = \frac{\tilde{n}_s}{\tilde{n}_0}, \quad \varsigma = \frac{\gamma\tilde{n}_0H^2}{D_C\Delta C}, \quad \tilde{n}_0 = \frac{1}{H} \int_0^H \tilde{n} d\tilde{z}, \quad (20)$$

where  $\tilde{n}_0$  is the average number density of the microorganisms. The constant  $A_1$  is the smallest positive root of the following transcendental equation:

$$\tan\left(\frac{1}{2}A_1\right) = \frac{\text{Pe}\varsigma}{A_1} \quad (21)$$

### 5. Linear stability analysis

The perturbations are introduced as follows:

$$\begin{aligned} [n, T, \mathbf{v}, p, C] = & [n_s(z), T_s(x, z), \mathbf{v}_s(U_s(z), 0, 0), p_s(z), C_s(z)] \\ & + [N(z), \Omega(z), \mathbf{V}(U(z), V(z), W(z)), P(z), \Xi(z)] \exp[i(kx + ly - \sigma t)] \end{aligned} \quad (22)$$

where,

$$y = \frac{\tilde{y}}{H}, \quad t = \frac{\tilde{t}\mu}{\rho H^2} \quad (23)$$

$k$  and  $l$  are the dimensionless wavenumbers in the  $x$ - and  $y$ -directions, respectively, and  $\sigma$  is the dimensionless disturbance frequency.

Substituting Equation (22) into the dimensionless version of Equations (1)-(5) and linearizing results in equations for the amplitudes  $U$ ,  $V$ ,  $W$ ,  $P$ ,  $N$ ,  $\Omega$ , and  $\Xi$ . The elimination of  $P$ ,  $U$ , and  $V$  from these equations for amplitudes gives the following equations for the remaining amplitudes  $W$ ,  $G$  ( $G$  is related to  $\Xi$  by first equation in (28)),  $N$ , and  $\Theta$  ( $\Theta$  is related to  $\Omega$  by third equation in (28)):

$$\begin{aligned} \frac{d^4 W}{dz^4} + [-2m^2 + i(\sigma - kU_s)] \frac{d^2 W}{dz^2} + \left[ m^4 + i \left( m^2 k U_s + k \frac{d^2 U_s}{dz^2} - m^2 \sigma \right) \right] W \\ = m^2 (\text{Ra}_B N - \text{Ra}_V \Theta) \end{aligned} \quad (24)$$

$$\begin{aligned} \left[ \frac{d^2}{dz^2} - \varpi \frac{dG_s}{dz} \frac{d}{dz} - \left( m^2 + i\text{Sc}(kU_s - \sigma) + \varpi \frac{d^2 G_s}{dz^2} \right) \right] N \\ = n_s \varpi \left( \frac{d^2 G}{dz^2} - m^2 G \right) + \frac{dn_s}{dz} \left( W + \varpi \frac{dG}{dz} \right) \end{aligned} \quad (25)$$

$$\left[ \frac{d^2}{dz^2} - (m^2 + i\text{Pr}(kU_s - \sigma)) \right] \Theta = \frac{dT_s}{dz} W \quad (26)$$

$$\left[ \delta \frac{d^2}{dz^2} - (\delta m^2 + i\text{Sc}(kU_s - \sigma)) \right] G = \delta N + W \frac{dG_s}{dz} \quad (27)$$

where,

$$G = \frac{\Xi}{\varsigma}, \quad G_s = \frac{C_s}{\varsigma}, \quad \Theta = \Omega \frac{\alpha}{D_N}, \quad \text{Ra}_B = \frac{gH^3 \Delta \rho \theta \tilde{m}_0}{\mu D_N} \quad (28)$$

$$\delta = \frac{D_C}{D_N}, \quad \varpi = \text{Pe}_\varsigma, \quad m^2 = k^2 + l^2, \quad \text{Sc} = \frac{\mu}{D_N \rho_w} \quad (29)$$

where  $\text{Ra}_B$  is the bioconvection Rayleigh number and  $\text{Sc}$  is the Schmidt number.

Steady-state solutions in Equations (24)-(28) are those given by Equations (14), (15), (18), and (19).

If both the lower and top boundaries are assumed rigid, Equations (24)-(27) must be solved subject to the following boundary conditions:

$$W = 0, \quad \frac{dW}{dz} = 0, \quad \Theta = 0, \quad G = 0, \quad \text{Pe} \left( n_s \frac{dG}{dz} + N \frac{dG_s}{dz} \right) = \frac{dN}{dz} \quad \text{at } z = 0 \quad (30)$$

$$W = 0, \quad \frac{dW}{dz} = 0, \quad \Theta = 0, \quad \frac{dG}{dz} = 0, \quad \frac{dN}{dz} = 0 \quad \text{at } z = 1 \quad (31)$$

If the top boundary is stress-free, second equation in (30) ( $dW/dz = 0$ ) must be replaced with the following equation:

$$\frac{d^2 W}{dz^2} = 0 \quad (32)$$

## 6. Numerical method and validation

The collocation method (Fletcher, 1984) is used for obtaining the numerical solution of the eigenvalue problem for Equations (24)-(27). For the case of the no-slip condition at the top surface (boundary conditions for this case are given by Equations (30) and (31)) the basis functions are:

$$W = \sum_{j=1}^M a_j z^{j+1} (1-z)^{j+1},$$

$$\Theta = \sum_{j=1}^M b_j z^j (1-z)^j,$$



$$N = 1 + \chi \sum_{j=1}^M c_j z^j (1 - z/2)^j,$$

$$G = \sum_{j=1}^M d_j z^j (1 - z/2)^j, \quad (33a, b, c, d)$$

where,

$$\chi = \frac{A_1(A_1 - \sin A_1)}{1 + \cos A_1} \quad (34)$$

( $M = 100$  is used in the numerical implementation of the code.)

For the case of the stress-free top boundary (see Equation (32)), Equation (33a) must be replaced with:

$$W = \sum_{j=1}^M a_j (z - 3z^3 + 2z^4)^{j+1} \quad (35)$$

The solution of the eigenvalue problem leads to the following dependence:

$$Ra_B = Ra_B(m, k, Ra_V, Ra_H, \varpi, Sc, Pr, \delta, \sigma) \quad (36)$$

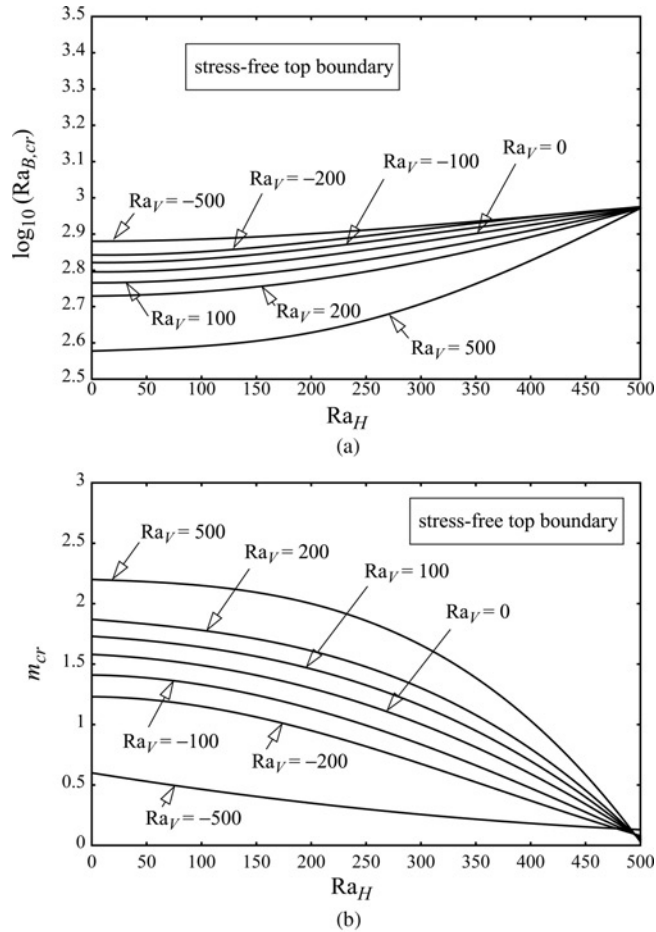
| $\delta$ | $\varpi$ | Hillesdon and Pedley (1996) |             | Present paper |             |
|----------|----------|-----------------------------|-------------|---------------|-------------|
|          |          | $m_{cr}$                    | $Ra_{B,cr}$ | $m_{cr}$      | $Ra_{B,cr}$ |
| 1        | 0.05     | 1.37                        | 10,200      | 1.38          | 10,237      |
| 1        | 1        | 1.58                        | 625         | 1.58          | 625         |
| 1        | 10       | 1.90                        | 200         | 1.90          | 200         |

**Notes:** Critical wavenumber obtained in this paper with that reported in Table III of Hillesdon and Pedley (1996), computations are performed for an isothermal layer with a stress-free top boundary

**Table I.**  
Comparison of the critical bioconvection Rayleigh number and wavenumber in this paper

| Parameter   | Definition                                       | Range or typical value |
|-------------|--|------------------------|
| Sc          | $(\mu/\rho_w)/D_N$                               | 7,700                  |
| Pr          | $(\mu/\rho_w)/\alpha$                            | 1-11                   |
| $\varsigma$ | $\gamma \tilde{m}_0 H^2 / D_C \Delta C$          | 43.75                  |
| Pe          | $W_c H / D_N$                                    | 0-37.5                 |
| $\varpi$    | $Pe \varsigma$                                   | 0-1,640                |
| $\delta$    | $D_C / D_N$                                      | 16                     |
| $Ra_V$      | $g \beta H^3 \Delta T \rho_w / \mu \alpha$       | 0-284,375              |
| $Ra_H$      | $g \beta H^4 \beta_H \rho_w / \mu \alpha$        | 0-7,200                |
| $Ra_B$      | $g H^3 \Delta \rho \theta \tilde{m}_0 / \mu D_N$ | 15,625                 |

**Table II.**  
Values of dimensionless parameters



**Figure 2.**  
The stress-free upper boundary case

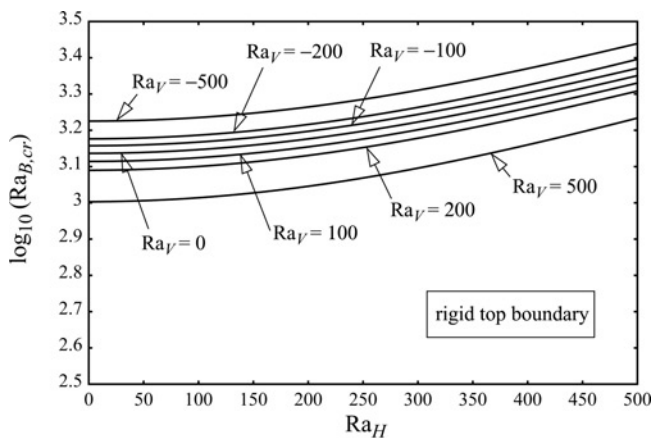
**Notes:** Effect of the horizontal Rayleigh numbers on the critical bioconvection Rayleigh number,  $Ra_{B,cr}$  (a) and on the critical wavenumber,  $m_{cr}$  (b)

for the bioconvection Rayleigh number. The critical bioconvection Rayleigh number is then obtained as:

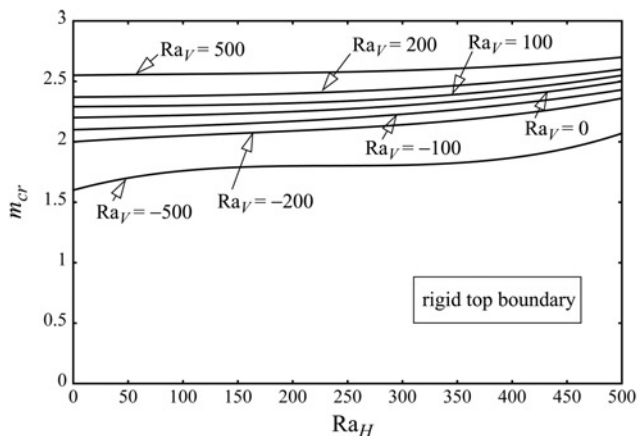
$$Ra_{B,cr} = \min\{Ra_B(m, k, Ra_V, Ra_H, \varpi, Sc, Pr, \delta, \sigma_i = 0)\} \quad (37)$$

where  $\sigma_i$  is the imaginary part of  $\sigma$ .

The collocation method for this eigenvalue problem is implemented utilizing the Matlab package. For validating the numerical code data obtained in Hillesdon and Pedley (1996) are used. Table I presents a comparison between the values of  $Ra_{B,cr}$  and  $m_{cr}$  that follow from Equations (24)-(27) and data of Hillesdon and Pedley (1996). Table I is for the case of the stress-free top surface (the only boundary condition considered in the above reference). There is an excellent agreement between the present computational results and data obtained in Hillesdon and Pedley (1996).



(a)

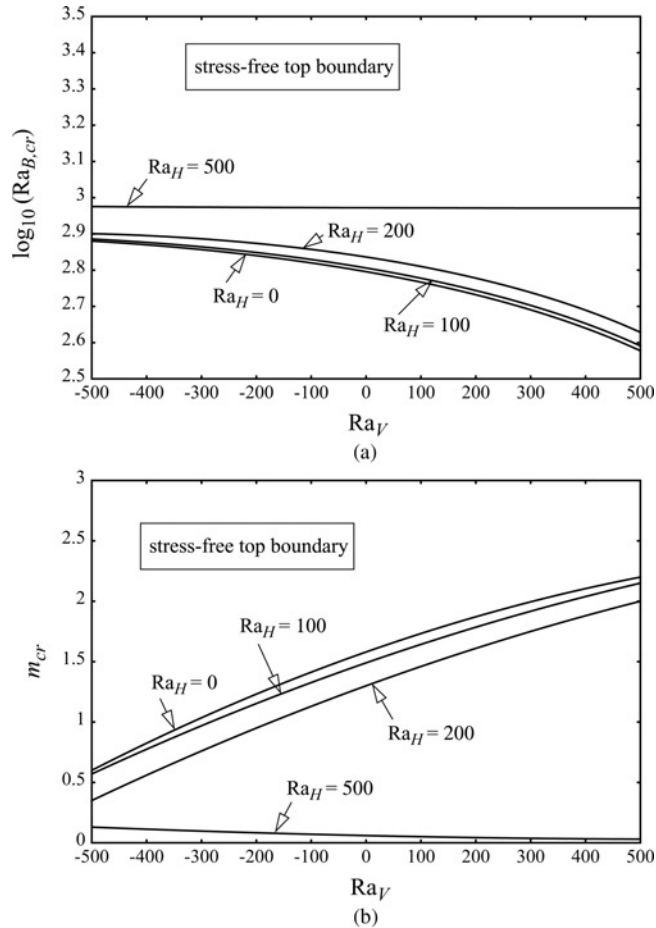


(b)

**Figure 3.**  
Same as Figure 2, the  
rigid upper boundary case

## 7. Results and discussion

Typical values of the dimensionless parameters for a soil bacterium *Bacillus subtilis* are estimated in Hillesdon and Pedley (1996) as follows:  $Pe = 15H$ ,  $\varsigma = 7H^2$ , and  $\delta = 16$ , where the layer depth,  $H$ , must be given in mm. A typical depth of a shallow layer in experiments described in Hillesdon *et al.* (1995) was 2.5 mm. For estimating the vertical and horizontal temperature gradients a  $10^\circ\text{C}$  temperature difference in both vertical and horizontal direction is assumed; the characteristic length in the horizontal direction is assumed to be 100 mm. The values of  $Ra_V$  and  $Ra_H$  should be understood as estimates of the maximum safe values of these parameters so that the temperature variation does not kill microorganisms; smaller values of  $Ra_V$  and  $Ra_H$  can be easily realized in a lab experiment. Using parameter values given in Hillesdon and Pedley (1996) and assuming that  $\tilde{n}_0 = 10^{15}$  cell/m<sup>3</sup>, an estimate of the range or a typical values of dimensionless parameters is given in Table II. Since the aim of this paper is not to study a particular biological system (not enough experimental data are available at this point to accomplish this task) but rather to investigate the trends,  $Ra_V = Ra_H = 100$ ,  $\varpi = 1$ , and  $Pr = Sc = 1$ , and  $\delta = 1$  are adopted as a basic case, and then

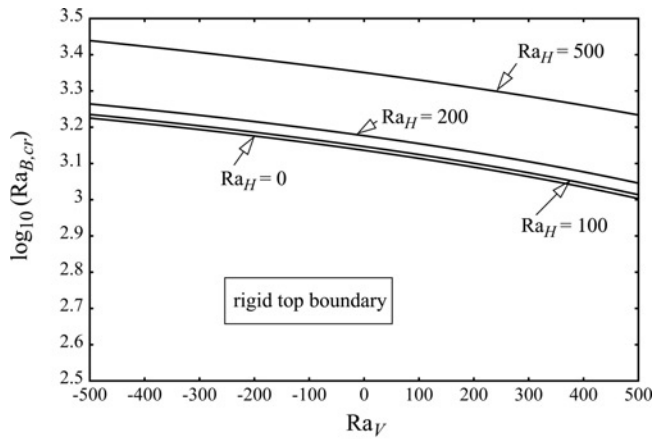


**Figure 4.**  
The stress-free upper  
boundary case

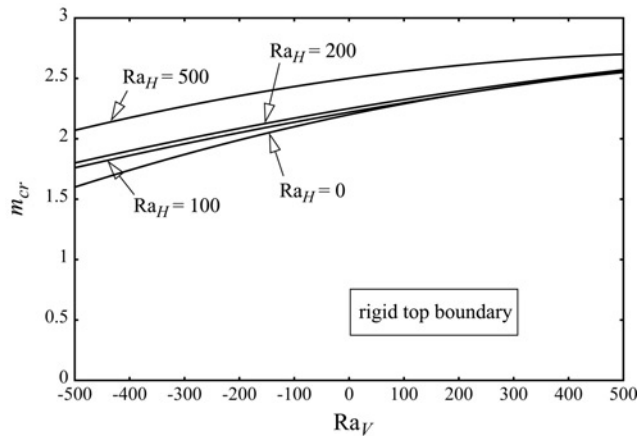
**Notes:** Effect of the vertical Rayleigh numbers on the critical bioconvection Rayleigh number,  $Ra_{B,cr}$  (a) and on the critical wavenumber,  $m_{cr}$  (b)

the values of  $Ra_V$ ,  $Ra_H$ ,  $\varpi$ ,  $Pr$ ,  $Sc$ , and  $\delta$  are varied around the basic case values in Figures 2-8.

Computational results for all parameter values investigated in this research indicate that the marginal state is stationary. This is in agreement with Hillesdon and Pedley (1996) who found no oscillatory marginal states for shallow chambers. Computational results presented in Figures 2 and 4 (stress-free top boundary) and Figures 3 and 5 (rigid top boundary) demonstrate the effects of the horizontal and vertical Rayleigh numbers on the bioconvection Rayleigh number. These results are computed for  $\varpi = 1$ ,  $\delta = 1$ , and  $Pr = Sc = 1$ . Figures 2a and 3a indicate that for both types of boundary conditions at the top surface the increase of the horizontal Rayleigh number stabilizes the system (increases the critical value of the bioconvection Rayleigh number). This suggests that the horizontal temperature gradient has the stabilizing effect on the system. This is explained as follows. The effect of increasing the



(a)

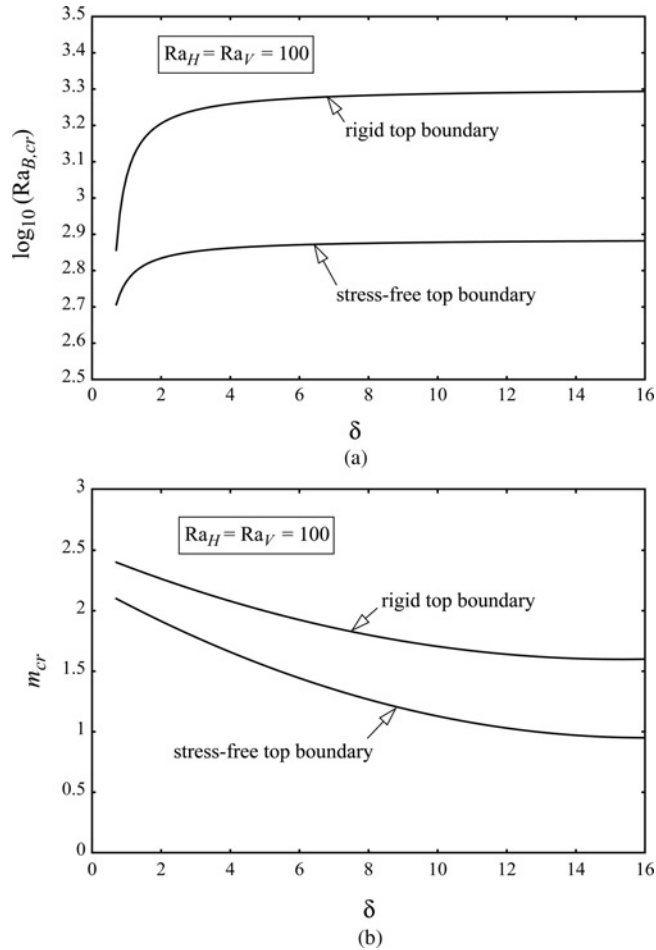


(b)

**Figure 5.**  
Same as Figure 4, the  
rigid upper boundary case

horizontal thermal Rayleigh number is to distort the basic temperature profile away from the linear one; this produces the stabilizing effect because the destabilizing vertical temperature gradient is decreased in magnitude in the bulk of the fluid. Figures 2b and 3b indicate that the increase of the horizontal Rayleigh number decreases the critical wavenumber for the stress-free top boundary and slightly increases the critical wavenumber for the rigid top boundary.

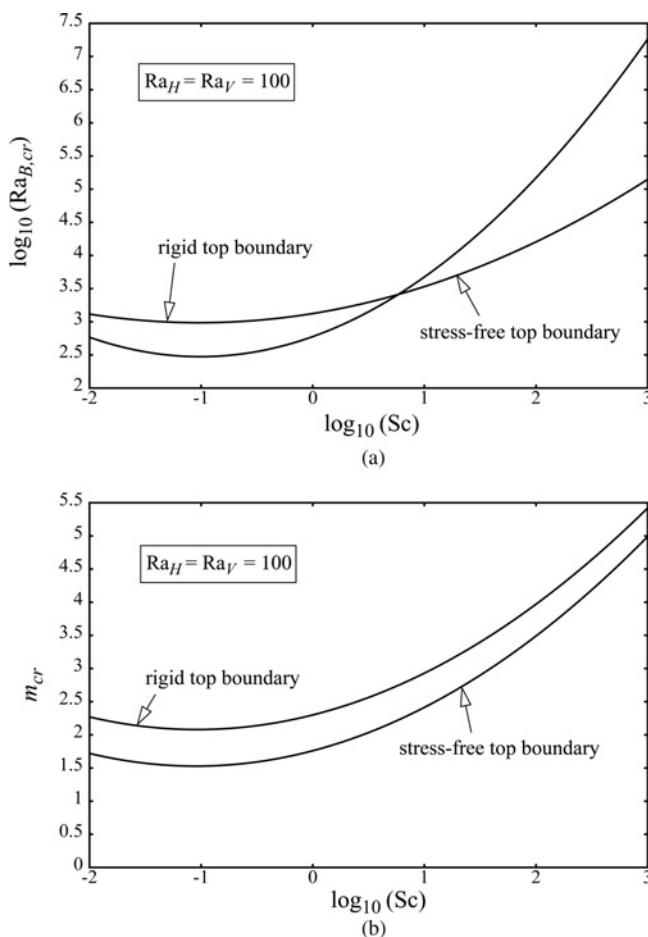
Figures 4a and 5a indicate that for both types of boundary conditions at the top surface and for all values of  $Ra_H$  considered in these computations the critical bioconvection Rayleigh number,  $Ra_{B,cr}$ , decreases with the increase of  $Ra_V$ . A similar trend is observed in Kuznetsov (2005a, b), where the case with no horizontal temperature gradient is investigated. This is as expected because increasing the vertical Rayleigh number means the increase of destabilizing effect of the vertical temperature gradient (positive values of the vertical Rayleigh number correspond to the negative vertical temperature gradient whose effect is destabilizing). The obtained results indicate that the boundary condition at the top surface strongly affects the behavior of the critical bioconvection Rayleigh number. For the stress-free top



**Figure 6.**  
Effect of  $\delta$  on the critical bioconvection Rayleigh number,  $Ra_{B,cr}$  (a) and on the critical wavenumber,  $m_{cr}$  (b)

boundary (Figure 4a) the effect of  $Ra_V$  on  $Ra_{B,cr}$  becomes less significant for large values of  $Ra_H$ . For example at  $Ra_H = 500$  the critical bioconvection Rayleigh number is almost independent of  $Ra_V$  (the corresponding curve in Figure 4a is a straight horizontal line). In contrast, for the rigid top surface (Figure 5a) the effect of  $Ra_V$  on  $Ra_{B,cr}$  remains significant even for  $Ra_H = 500$ . Figures 4b and 5b indicate that the increase of the horizontal Rayleigh number increases the critical wavenumber for both the stress-free and rigid top boundary cases (except for the large horizontal Rayleigh number case,  $Ra_H = 500$ , in which case  $m_{cr}$  is almost independent of  $Ra_V$  for the stress-free top boundary).

The effect of  $\delta$  on the critical bioconvection Rayleigh number is displayed in Figure 6a; the results are computed for  $Ra_V = Ra_H = 100$ ,  $\varpi = 1$ , and  $Pr = Sc = 1$ . The increase of  $\delta$  stabilizes the basic flow. It can be explained as follows. Increased value of  $D_C$  corresponds to more uniform oxygen distribution, smaller gradient of oxygen concentration, and, according to Equation (7), less vigorously swimming microorganisms. Since upswimming of microorganisms causes the unstable density stratification, less vigorously swimming microorganisms result in a more stable basic flow. Figure 6b

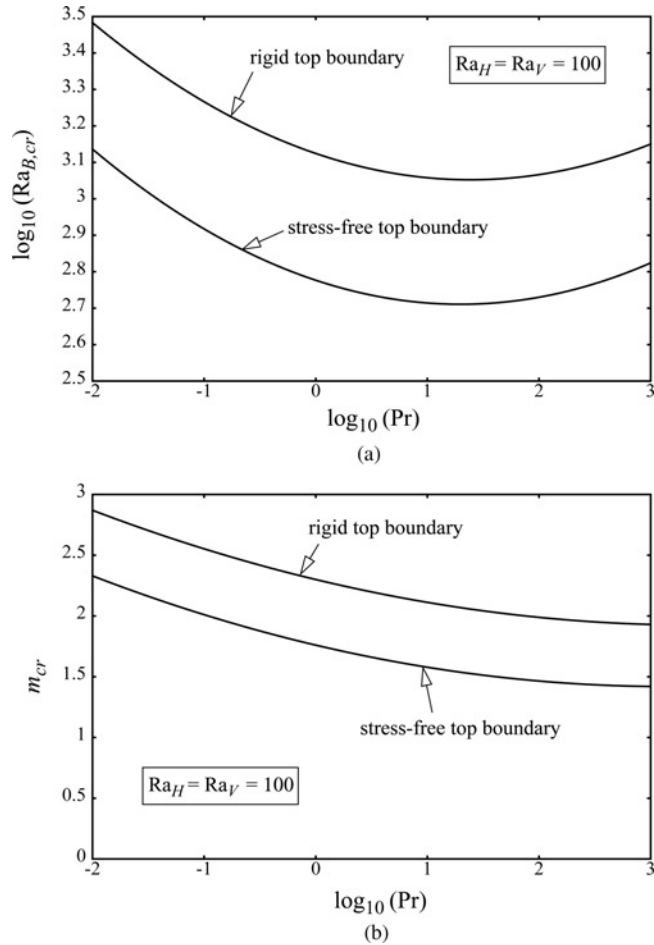


**Figure 7.** Effect of  $Sc$  on the critical bioconvection Rayleigh number,  $Ra_{B,cr}$  (a) and on the critical wavenumber,  $m_{cr}$  (b)

shows that the increase of  $\delta$  decreases the critical wavenumber for both types of boundary conditions at the top surface.

The effect of the Schmidt number on the critical bioconvection Rayleigh number is shown in Figure 7a; the results are computed for  $Ra_V = Ra_H = 100$ ,  $\varpi = 1$ ,  $\delta = 1$ , and  $Pr = 1$ . The increase of the Schmidt number stabilizes the basic flow; the effect is most pronounced for large values of  $Sc$ . The increase of the Schmidt number also generally increases the critical wavenumber (Figure 7b).

The effect of the Prandtl number on the critical bioconvection Rayleigh is shown in Figure 8; the results are computed for  $Ra_V = Ra_H = 100$ ,  $\varpi = 1$ ,  $\delta = 1$ , and  $Sc = 1$ . The trend of increasing the Prandtl at lower  $Pr$  destabilizes the basic flow, while at larger Prandtl numbers the increase in  $Pr$  stabilizes the flow. In Figure 8a the switch from destabilizing to stabilizing occurs for the rigid to surface at around  $Pr = 50$  and for the stress-free case at around  $Pr = 15$ . The increase of the Prandtl number also decreases the critical wavenumber.



**Figure 8.** Effect of  $Pr$  on the critical bioconvection Rayleigh number,  $Ra_{B,cr}$  (a) and on the critical wavenumber,  $m_{cr}$  (b)

### 8. Conclusions

Linear stability analysis of the combined bioconvection and thermal instability problem in a horizontal layer of finite depth occupied by a suspension of oxytactic microorganisms in which the basic temperature gradient is inclined to the vertical is carried out.

The increase of the horizontal thermal Rayleigh number (when the vertical thermal Rayleigh number is kept constant) stabilizes the basic flow. The effect of increasing the horizontal thermal Rayleigh number is to distort the basic temperature profile away from the linear one.

The increase of the Schmidt number stabilizes the basic flow. The increase of the Prandtl number first causes the bioconvection Rayleigh number to decrease and then to increase; the dependence  $Ra_B(Pr)$  thus exhibits a minimum for both stress-free and rigid top boundaries.

The increase of  $\delta$  stabilizes the basic flow because an increased value of  $D_C$  corresponds to more uniform oxygen distribution, smaller gradient of oxygen concentration, and less vigorously swimming microorganisms.



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